

June 10, 2016

Mr. Mark Gunn, P.E. Rinker Design Associates, P.C. 9385 Discovery Boulevard, Suite 200 Manassas, Virginia 20109

Reference: Addendum Letter - Minor Structure Report for Retaining Wall RW #1 **Sycolin Road Widening Phase IV** VDOT Project No. U000-253-312, P101, R201, C501 Leesburg, Virginia DMY Project No. 01.02095.01

Dear Mr. Gunn:

DMY Engineering Consultants Inc. (DMY) is pleased to submit this addendum letter to our Geotechnical Engineering Report dated August 21, 2015 (latest revision May 25, 2016) for the above-referenced project. This letter presents a minor structure report for Retaining Wall RW #1.

1.0 **PROJECT INFORMATION**

Retaining Wall RW #1 is proposed on the east side of Sycolin Road from Station 116+50 to Station 118+80. The height of the retaining wall varies from 7 to 16 feet (from bottom of footing to top of wall) with an exposed height varying from 0 to 11 feet. The proposed retaining wall is located on an existing 2H:1V slope with height varying from 12 to 17 feet. The type of retaining wall was not determined at the time of report preparation. It appears that either a segmental block MSE wall or a cantilever concrete wall is suitable. The retaining wall and associated soil boring information is summarized in the following table:

Wall ID	Location	Retaining Wall Type	Max. Exposed Wall Height (feet)	Reference Borings
RW #1	Sycolin Road Sta. 116+50 to 118+80, Right	MSE/Cantilever	11	RW-1 through RW-5

Table 1-1: Summa	ry of Retaining Wall
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45662 Terminal Drive, Suite 110, Dulles, Virginia 20166 • www.dmyec.com • Phone: (703) 665-0586 • Fax: (202) 688-1918

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The description of the proposed project given above is based on the information provided to us by the project team and information gathered during our site reconnaissance. If any of the assumptions or project information is incorrect or changed, DMY should be informed so that we may revise our geotechnical recommendations, if necessary.

2.0 SITE GEOLOGY AND SUBSURFACE CONDITIONS

2.1. Site Geology

Based on a review of the Virginia Geologic Map Data available through USGS's online resources (<u>http://mrdata.usgs.gov/geology/state/state.php?state=VA</u>), the project site is located within the Culpeper Basin of Northern Virginia and is underlain by Newark Supergroup including Sandstone, Siltstone and Shale of the Upper Triassic Age.

In the Culpeper Basin, residual soils have developed from the in-place chemical and physical weathering of the underlying parent bedrock. The soils associated with this geology typically consist of sandy clays, silts, and silty sand materials along with varying amounts of weathered rock fragments. With increasing depth, soil increases in granularity and strength, gradually transitions into highly weathered or Intermediate Geomaterials, and eventually transitions into competent bedrock.

The subsurface profile may be altered by man, by excavating or filling, or by effects of water through the process of erosion or alluvial deposition.

2.2. Subsurface Conditions

A total of five (5) Standard Penetration Test (SPT) borings (RW-1 through RW-5) were drilled at the proposed retaining wall. The borings were drilled by a track-mounted CME-55 drill rig using the hollow stem auger method with automatic hammer. The approximate locations of the borings are shown on the attached Boring Location Plan. The subsurface conditions encountered at the boring locations are shown in the attached boring logs.

Surficial Materials

About 4 inches of topsoil was encountered in all borings.

Residual Soils

Immediately beneath the surficial soils, residual soils were encountered in all borings. The encountered residual soils in the borings consisted of soft to stiff sandy SILT (ML) and medium dense to very dense silty SAND (SM) and clayey SAND (SC) with SPT N-values ranging from 4 to 67 blows per foot (bpf). Varying amounts of rock fragments were present in the soil samples.

Intermediate Geomaterials (IGM)

IGM is defined as natural residual soils having a minimum SPT N-value of 50 blows per 6 inches of penetration. IGM was encountered in all borings and consisted of very dense silty SAND (SM) with varying amounts of rock fragments.

Auger Refusal Materials

Auger refusal was encountered in Borings RW-1 through RW-4 at depths ranging 7.5 to 16 feet below site grade corresponding to EL 358.1 to EL 378.0 feet. Auger refusal materials could be parent bedrock, boulder, or lens of rock.

Groundwater

Groundwater was not encountered either during drilling or at 24 hours after drilling completion. It should be noted that groundwater levels fluctuate with seasonal and climatic variations and may be different at other times and locations than those stated in this letter.

3.0 RETAINING WALL RECOMMENDATIONS

The soil parameters used for the evaluation are summarized in the following table. These parameters were selected based on our current subsurface exploration, *VDOT's Soil Design Parameters for Sound Barrier Walls, Retaining Walls, and Non-Critical Slopes,* our prior experience in similar soils and geologies, and laboratory testing results. The laboratory testing results are included in the attachment.

Soil Stratum	Soil Classification	Range of SPT N ₆₀ (bpf)	Cohesion, c (psf)	Friction Angle, ∳ (degree)	Moist Unit Weight (pcf)	Saturated Unit Weight (pcf)
New Fill	ML, SC, or SM	-	50	30	115	122
Residual-I	ML & SC	4 to 15	250	20	110	117
Residual-II	SM & SC	25 to 67	100	34	130	137
IGM	SM	50/6" to 50/1"	250	36	132	139

Table 3-1: Summary Soil Parameters

We have evaluated the wall foundation bearing capacity and settlement at the maximum wall height location. In our evaluation, we assumed a minimum footing width (for cantilever wall) or a minimum reinforcement length (for MSE wall) of 9.6 feet at the location of maximum wall height. The nominal and factored foundation bearing capacity was determined to be 10,920 PSF and 4,914 PSF, respectively. A resistance factor of 0.45 was used. The detailed calculations are attached to the end of this letter.

A detailed global stability analysis was not performed; however, considering the dense to very dense nature of the onsite soils, the presence of shallow auger refusal materials, and our engineering experience of nearby sites with similar geology, global stability is not considered an issue at this site.

Based on our subsurface exploration data and our analyses, no undercut and replacement are required. IGM was encountered at or above the proposed foundation elevations. Difficult excavation involving a large trackhoe equipped with a hoe ram is likely needed to achieve the proposed grades.

All new footings should be placed at a minimum depth of 30 inches below finished grade to provide adequate frost cover protection acceptable for this region. Heavy earthwork equipment should maintain a minimum horizontal distance away from the walls of one foot per foot of vertical wall height. Lighter compaction equipment should be used close to the walls.

During construction, the bearing capacity at the final footing excavation should be documented in the field by an authorized representative of the Geotechnical Engineer of Record to check that the in situ bearing capacity at the bottom of each footing excavation is adequate for the design loads.

4.0 LIMITATIONS

The recommendations provided are based in part on project information provided to us and are only applied to the specific project and site discussed in this letter. If the project information section in this letter contains incorrect information or if additional information is available, DMY should be contacted to review our recommendations. We can then modify our recommendations for the proposed project.

Regardless of the thoroughness of a subsurface investigation, there is always a possibility that subsurface conditions may vary from those documented during a subsurface exploration at specific locations. In addition, the construction process itself may alter subsurface conditions. Therefore, experienced geotechnical personnel should be engaged to observe and document the construction procedures used and the conditions encountered. Unanticipated conditions and inadequate procedures should be reported to the design team along with timely recommendations. We recommend that DMY be retained to provide this service based upon our familiarity with the project, the subsurface conditions, and the intent of the recommendations.

We have prepared this letter for use by the design professionals for design purposes in accordance with generally accepted geotechnical engineering practices. No other warranty, expressed or implied, is made as to the professional advice included in this letter.

We appreciate the opportunity to be of service to you on this project and please do not hesitate to contact the undersigned if you have any questions regarding the information in this letter. We look forward to serving as your geotechnical engineer on the remainder of this project and on future projects.

Respectfully,

DMY ENGINEERING CONSULTANTS

Paul Li, PhD, PE Project Engineer

Attachments:

ANTS INC. PENG ZHANG Lic. No. 048994 06/10/2016 06/10/2016 Peng "Paul" Zhang, PE Vice President

Boring Location Plan Boring Logs Laboratory Test Results Retaining Wall Calculations



THESE PLANS ARE UNFINISHED AND UNAPPROVED AND ARE NOT TO BE USED FOR CONSTRUCTION.

ADDITIONAL EASEMENTS FOR UTILITY RELOCATIONS MAY BE REQUIRED BEYOND THE PROPOSED RIGHT-OF-WAY SHOWN ON THESE PLANS.



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REVISED 10/11/2013

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									STRUCTURE: RETAINING WALL	P	AG	E 1 ()F 1
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3.0 3.5 4.0	382	5 7 10	100	4					4.0/381.46	36	8	24.3	97.7
4.5 5.0 5.5	- 380	8 16 39 50/4	109						<i>Residual</i> , Brown, fine to medium, SILTY SAND, very dense, moist SM	-		13.7	
6.0 6.5 7.0	-	50/4	100	5.83 6 6.33					<i>IGM</i> , Brown, fine to coarse, SILTY SAND WITH GRAVEL, very dense, moist SM			11.4	
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Vigth: Department of Transportation STRUCTURE: RETAINING WALL PAGE 1 OF 1 STRUCTURE: 820 07145" N SURFACE ELEVATION: 368.79 ft OFFSET: R.80 LONGITUDE: 77.552386" W COORD. DATUM: NAD 83 Image: Structure in the structur											PROJECT #: U000-253-312 P101,R201, C501 LOCATION: Leesburg, VA		R	N- :	3
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4		20 28	84										9.0	
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		16 12	100										25.3	
. 8 -	360	50/5	100	8 8.42						8.0 / 360.62 <i>IGM</i> , Light brown, fine to coarse, SILTY SAND WITH GRAVEL, very dense, moist SM			11.4	
10 -										10.5 / 358.12				
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1.0		8	75	M						Residual, Brown and gray, SANDY SILT, stiff, moist ML			18.4	
1.5	382	10												
2.0		34		2						2.0 / 381.51	1			
2.5		46	67	V						Residual, Gray, fine to coarse, SILTY SAND WITH GRAVEL,			16 1	
3.0		40	07	A						SAME contains rock fragments			10.1	
3.5	380	50/6		3.5										
4.0				4										
4.5		16												
5.0		31	100	Y									19.4	
5.5	378	36		A										
6.0	010	41		6										
6.5		16		Ň										
0.5		20	85	Å									23.3	
[7.0]		50/2	ŀ	7.17						7.0 / 376.51]			
1.5	376	-								contains rock fragments, very dense, moist SM				
8.0		50/2	100	× 8 8.17									6.1	
8.5		-												
9.0														
9.5	374	-												
10.0										10.0 / 373.51	-			
										Boring Terminated at 10 feet.				
2														
5 j														
	IARKS	Rig Type:	CME	55.								10)F 1	
Tem	porary	piezométer	was ir	nstalled	l to 1	10 ft a	nd s	cree	ened	for bottom 5 ft for 24-hr ground water readings.			· · ·	
	ight 201	6. Commonwea	alth of \	/irginia								v - C)	

SPT_LOG:LOGS.GPJ:8.30.003:012512:5/25/16



Dulles, Virginia 20166 tel: (703) 665-0586 fax: (202) 688-1918

DMY ENGINEERING CONSULTANTS INC. SUMMARY OF LABORATORY RESULTS 45662 Terminal Drive, Suite 110

PAGE 1 OF 1

PROJECT NAME Sycolin Road Retaining WALL

CLIENT Rinker Design Associates, P.C.

01.02095.	01					PROJECT LOCATION Town of Leesburg, Virginia							
Depth (FT)	Liquid Limit	Plastic Limit	Plasticity Index	%<#200 Sieve	Water Content (%)	Proctor Method	Max Dry Density (pcf)	Optimum Moisture (%)	Oversize Fraction (%)	Sample Description/Classification			
0.0 - 2.0					20.6								
2.0 - 4.0	36	28	8	97.7	24.3					Brown, Silt (ML)			
4.0 - 6.0					13.7								
6.0 - 8.0					11.4								
0.0 - 2.0					21.7								
2.0 - 4.0	32	21	11	44.0	14.1					Brown, Clayey Sand (SC)			
4.0 - 6.0					9.9								
6.0 - 8.0					6.6								
8.0 - 10.0					4.5								
13.5 - 15.0					9.0								
0.0 - 2.0					23.1								
2.0 - 4.0					8.9								
4.0 - 6.0					7.0								
6.0 - 8.0	NP	NP	NP	15.1	17.4					Brown, Silty Sand With Gravel (SM)			
0.0 - 2.0					6.6								
2.0 - 4.0	NP	NP	NP	35.0	8.2					Brown, Silty Sand With Gravel (SM)			
4.0 - 6.0					9.0								
6.0 - 8.0					25.3								
8.0 - 10.0					11.4								
0.0 - 2.0					18.4								
2.0 - 4.0					16.1								
4.0 - 6.0					19.4								
6.0 - 8.0					23.3								
8.0 - 10.0					6.1								
	01.02095. Depth (FT) 0.0 - 2.0 2.0 - 4.0 4.0 - 6.0 6.0 - 8.0 2.0 - 4.0 4.0 - 6.0 6.0 - 8.0 8.0 - 10.0 13.5 - 15.0 0.0 - 2.0 2.0 - 4.0 4.0 - 6.0 6.0 - 8.0 0.0 - 2.0 2.0 - 4.0 4.0 - 6.0 6.0 - 8.0 0.0 - 2.0 2.0 - 4.0 4.0 - 6.0 6.0 - 8.0 8.0 - 10.0 0.0 - 2.0 2.0 - 4.0 4.0 - 6.0 8.0 - 10.0 0.0 - 2.0 2.0 - 4.0 4.0 - 6.0 8.0 - 10.0 6.0 - 8.0 8.0 - 10.0	Ot.02095.01 Depth (FT) Liquid Limit 0.0 - 2.0 2.0 - 4.0 2.0 - 4.0 36 4.0 - 6.0 0 6.0 - 8.0 0 2.0 - 4.0 32 4.0 - 6.0 0 6.0 - 8.0 0 3.0 - 10.0 13.5 - 15.0 0.0 - 2.0 2.0 - 4.0 4.0 - 6.0 0 6.0 - 8.0 NP 0.0 - 2.0 2.0 - 4.0 4.0 - 6.0 0 6.0 - 8.0 NP 0.0 - 2.0 2.0 - 4.0 2.0 - 4.0 NP 0.0 - 2.0 2.0 - 4.0 2.0 - 4.0 NP 0.0 - 2.0 2.0 - 4.0 2.0 - 4.0 1.0 - 6.0 6.0 - 8.0 2.0 - 4.0 4.0 - 6.0 1.0 - 6.0 2.0 - 4.0 1.0 - 6.0 2.0 - 4.0 1.0 - 6.0 6.0 - 8.0 1.0 - 6.0 6.0 - 8.0 1.0 - 6.0 6.0 - 8.0 1.0 - 6.0 6.0 - 8.0	Depth (FT) Liquid Limit Plastic Limit 0.0 - 2.0 2 2.0 - 4.0 36 28 4.0 - 6.0 - - 6.0 - 8.0 - - 2.0 - 4.0 32 21 4.0 - 6.0 - - 6.0 - 8.0 - - 8.0 - 10.0 - - 13.5 - 15.0 - - 0.0 - 2.0 - - 2.0 - 4.0 - - 13.5 - 15.0 - - 0.0 - 2.0 - - 2.0 - 4.0 NP NP 0.0 - 2.0 - - 2.0 - 4.0 NP NP 0.0 - 2.0 - - 2.0 - 4.0 NP NP 4.0 - 6.0 - - 6.0 - 8.0 - - 8.0 - 10.0 - - 2.0 - 4.0 - - 2.0 - 4.0 - - <tr< td=""><td>Depth (FT) Liquid Limit Plastic Limit Plasticty Index 0.0 - 2.0 2.0 - 4.0 36 28 8 4.0 - 6.0 0.0 - 2.0 0.0 - 2.0 0.0 - 2.0 2.0 - 4.0 32 21 11 4.0 - 6.0 6.0 - 8.0 8.0 - 10.0 13.5 - 15.0 0.0 - 2.0 2.0 - 4.0 4.0 - 6.0 0.0 - 2.0 2.0 - 4.0 NP NP 4.0 - 6.0 6.0 - 8.0 0.0 - 2.0 <</td><td>Depth (FT)Liquid LimitPlastic LimitPlasticity Index%<#200 Sieve$0.0 - 2.0$$2.0 - 4.0$3628897.7$4.0 - 6.0$$6.0 - 8.0$$0.0 - 2.0$$2.0 - 4.0$32211144.0$4.0 - 6.0$$6.0 - 8.0$$8.0 - 10.0$$13.5 - 15.0$$0.0 - 2.0$$2.0 - 4.0$$4.0 - 6.0$$6.0 - 8.0$NPNPNP$15.1$$0.0 - 2.0$$2.0 - 4.0$NPNP$1.0 - 6.0$$8.0 - 10.0$$2.0 - 4.0$$4.0 - 6.0$$2.0 - 4.0$$4.0 - 6.0$$6.0 - 8.0$$8.0 - 10.0$$8.0 - 10.0$$4.0 - 6.0$<t< td=""><td>0.02095.01Depth (FT)Liquid LimitPlastic LimitPlasticity Index%<#200 SieveWater Content (%)$0.0 - 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6.0$ $ 8.0 - 10.0$ $ 2.0 - 4.0$ $ 4.0 - 6.0$ $ 2.0 - 4.0$ $ 4.0 - 6.0$ $ 4.0 - 6.0$ $ 4.0 - 6.0$ $ 4.0 - 6.0$ $ 4.0 - 6.0$ $ 4.0 - 6.0$ $ 6.0 - 8.0$ $ 8.0 - 10.0$ $ 8.0 - 10.0$ $ 4.0 - 6.0$ <t< td=""><td>0.02095.01Depth (FT)Liquid LimitPlastic LimitPlasticity Index%<#200 SieveWater Content (%)$0.0 - 2.0$22220.620.6$2.0 - 4.0$3628897.724.3$4.0 - 6.0$1111.411.4$0.0 - 2.0$211144.014.1$0.0 - 2.0$211144.014.1$0.0 - 2.0$211144.014.1$0.0 - 2.0$211144.014.1$4.0 - 6.0$2114.59.9$6.0 - 8.0$2114.59.0$0.0 - 2.0$2119.09.0$0.0 - 2.0$21117.4$2.0 - 4.0$NPNPNP15.117.4$0.0 - 2.0$21114.1$0.0 - 2.0$21114.1$0.0 - 2.0$21114.1$0.0 - 2.0$3339.0$6.0 - 8.0$NPNPNP35.08.2$4.0 - 6.0$44414.1$0.0 - 2.0$2223$8.0 - 10.0$44414.1$0.0 - 2.0$44414.1$0.0 - 2.0$44414.1$0.0 - 2.0$44414.1$0.0 - 8.0$4</td></t<> <td>Depth (FT)Liquid LimitPlastic LimitPlasticity Index%<#200 SieveWater Content (%)Proctor Method0.0 - 2.020.62.0 - 4.03628897.724.34.0 - 6.013.76.0 - 8.011.40.0 - 2.021.72.0 - 4.032211144.014.14.0 - 6.09.96.0 - 8.06.68.0 - 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GRAIN SIZE



Shallow Foundation Bearing Capacity Calculations

Project Number:	VDOT No. U000-253-312, P101, R201, C501; DMY No. 01.02095.01						
Project Name:	Sycolin R	load Widen	ing				
Project Location:	Leesburg	g, Virginia					
Foundation Location:	Retainin	g Wall RW 🕯	#1; Station 117+25				
Reference Borings:	RW-2						
Eccentricity=	1.6	ft					
B =	9.6	ft	Soil Type: SM				
Y =	130	pcf					
Y _{sat} =	137	pcf	Reference: Soil Design Parameter for Sound Barrier				
φ =	34	degrees	walls, Retaining Walls and Non-critical Slopes,				
c =	100	psf	VDOT April 2011				
D _f =	3.0	ft					
N=	25 to 67	blows/ft					

Bearing Capacity for Continuous or Strip Foundation

$q_u =$	$c'N_c + qN_q +$	$\frac{1}{2}\gamma B N_{\gamma}$
where,	$q = \gamma * D_f$	-
	Nc =	5.2
	Nq =	0.0
	Ny =	25.0
Res	sistance Factor =	0.45

Nominal Bearing q_u=

Factored Bearing q_a= 4914

Reference: Principle of Foundation Engineering 6th Edition, Chapter 3, Braja M. Das

LRFD Manual Table 10.6.3.1.2a-1; Bearing capacity factors reduced for footing on slope. Fig. 10.6.3.1.2c-1 and 10.6.3.2c-2

LRFD Manual Table 11.5.7-1

Calculated by:	PL	6/7/2016
Checked by:	ΡZ	6/10/2016

psf

psf

10920

Settlement Estimate -Burland & Burbidge

Wall Footing (Strip) (Station 117+25)

(0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.		
· · · · · ·		EN
Footing Width (ft)	В	9.6
Footing Length (ft)	L	100
Depth of Influence (ft)	Zı	7.3
N average within Z _I	N60	25
Preconsolidation Pressure (psf)	σ _p '	0
Structrual Load (plf)	P	47040
Bearing Pressure (psf)	q	4900

Footing Shape Factor	Fs	1.5
Settlement (inch)	S	0.6